



Impact of irradiation on the surface recombination velocity of a back side monochromatic illuminated bifacial silicon solar cell under frequency modulation

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Abstract In a dynamic frequency regime, the effect of irradiation on the bulk and surface recombination parameters (S_f , S_b) occurring in the bifacial photovoltaic cell monochromatically back-illuminated is presented. From the resolution of the continuity equation, through the photocurrent plots, we end with the expressions of S_f and S_b . Equivalent electric models related to S_f and S_b are deduced from Nyquist and Bode diagrams of the latter for some irradiation energy values. And subsequently, a method for determining equivalent electric parameters is proposed.

Keywords Irradiation-frequency modulation-recombination velocity-Bode and Nyquist diagram

1. Introduction

Solar cells are subject to a constant bombardment of high subatomic energy particles (electrons and protons). Thus, Electronic systems operating in space are exposed to radiation in the form of energetic charged particles, such as protons and heavy ions [1]. Indeed, irradiation of these cells generates atomic displacements within the material. Point defects resulting from these displacements trap the minority electric charge carriers produced by the illumination, which reduces the collection efficiency of the charges and alters the electrical characteristics of the cells (maximum power P_m , short circuit current J_{SC} and voltage in open circuit V_{OC}) [2]. Researchers have thus always carried out extensive studies in order to control and improve the behaviour of solar cells in such a hostile (irradiated) environment [3].

In this paper, the study deals with the impact of irradiation on the recombination parameters of a backside illuminated (BSI) bifacial photovoltaic cell under monochromatic light. First, we make a theoretical study to bring out all the mathematical equations for this type of photovoltaic cell. Then, using Nyquist and Bode diagrams [4-5], we put forward equivalent electrical model [6] for a few irradiation energy values. And in the end, a method for determining electric parameters relating to surface recombination velocities S_f and S_b will be proposed.

2. Theoretical Study

Our solar cell is made up of polycrystalline silicon [7-10], n^+p-p^+ type [11-12], with Back Surface Field (BSF) [13-14] whose structure is shown in the following figure.



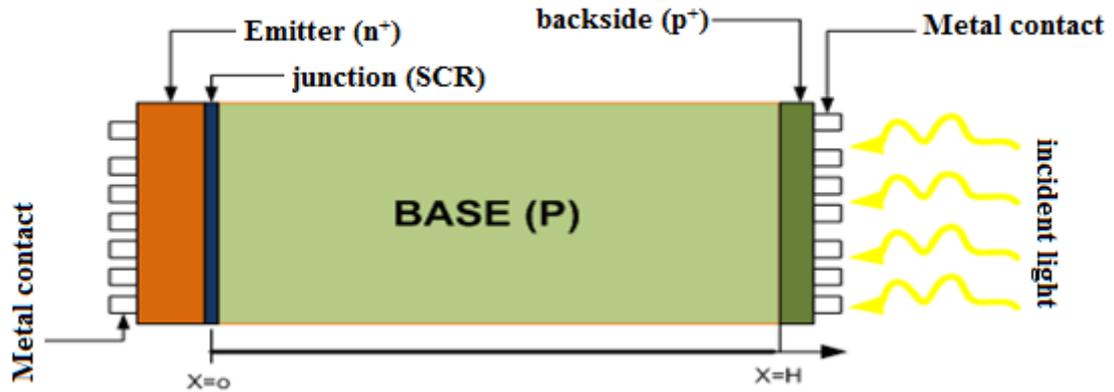


Figure 1: An n+-p-p+ structure of a silicon solar cell: backside illumination

This work is carried out with the assumptions that:

- ✓ the contribution of the emitter is neglected,
- ✓ the base is a quasi-neutral base (QNB)
- ✓ we use one-dimensional mathematical model. The origin is taken at the junction.

From these assumptions, the continuity equation is given in the following equation.

$$D(kl, \phi) \cdot \frac{\partial^2 \delta(x, t)}{\partial x^2} - \frac{\delta(x, t)}{\tau} = -G(x, t) + \frac{\partial \delta(x, t)}{\partial t} \tag{1}$$

$G(x, t)$ and $\delta(x, t)$ are respectively the global generation rate and the excess minority density carriers at position x and time t and can be written in the form as follows [15-19]:

$$G(x, t) = g(x)e^{i\omega t} \text{ et } \delta(x, t) = \delta(x)e^{i\omega t} \tag{2}$$

where, $g(x)$ and $\delta(x)$ typify the spatial components, $e^{i\omega t}$ the temporal component. Inserting equation (2) in equation (1) one obtains:

$$\frac{\partial^2 \delta(x)}{\partial x^2} - \frac{1}{L(\omega, kl, \phi)^2} \cdot \delta(x) = - \frac{g(x)}{D(kl, \phi)} \tag{3}$$

With,

$$\frac{1}{L^2(\omega, kl, \phi)} = \frac{1}{L^2(kl, \phi)} (i\omega\tau + 1) \quad \text{And} \quad D(kl, \phi) = \frac{L^2(kl, \phi)}{\tau(kl, \phi)}$$

for this type of solar cell, the spatial component of the minority carrier generation rate is given by the expression (4):

$$g(x) = \alpha I_0 (1 - R) e^{-\alpha(H-x)} \tag{4}$$

L_ω is the complex diffusion length [20]; $\alpha(\lambda)$ is the monochromatic optical absorption coefficient [21] at the wavelength λ ; $R(\lambda)$ is the reflection coefficient of the material at the wavelength λ ; H the thickness of the base. D is the complex diffusion coefficient; ω is the angular frequency; τ is the average lifetime of the minority carriers obtained from the empirical relation as a function of the damage coefficient kl and the irradiation flux ϕ [22-23].



$$\frac{\mathbf{1}}{\tau} = \frac{\mathbf{1}}{\tau_0} + kl.\phi \quad (5)$$

The solution of the continuity equation is given by the following expression:

$$\delta(x) = A \cosh\left(\frac{x}{L_\omega}\right) + B \sinh\left(\frac{x}{L_\omega}\right) + \frac{\alpha.I_0.(1-R).L_\omega^2}{D.(1-\alpha^2.L_\omega^2)} \cdot \exp-\alpha(H-x) \quad (6)$$

Where coefficients A and B are to be determined from the boundary conditions at the junction and to the rear side [24].

▪ At the Junction (x=0)

$$\left. \frac{\partial \delta(x)}{\partial x} \right)_{x=0} = S_f \cdot \frac{\delta(0)}{D} \quad (7)$$

▪ At the backside (x=H)

$$\left. \frac{\partial \delta(x)}{\partial x} \right)_{x=H} = -S_B \cdot \frac{\delta(H)}{D} \quad (8)$$

all calculation done, we get.

$$A_2 = \frac{\alpha.I_0.(1-R).L_\omega^3 \left\{ -D.(\alpha.D + S_B) - (-\alpha.D + S_f) \left[D.\cosh\left(\frac{H}{L_\omega}\right) + L_\omega.S_B.\sinh\left(\frac{H}{L_\omega}\right) \right] e^{-\alpha H} \right\}}{D.(1-\alpha^2.L_\omega^2) \left[L_\omega.D(S_B + S_f).\cosh\left(\frac{H}{L_\omega}\right) + (D^2 + S_f.S_B.L_\omega^2) \sinh\left(\frac{H}{L_\omega}\right) \right]} \quad (9)$$

$$B_2 = \frac{\alpha.I_0.(1-R).L_\omega^3 \left\{ -L_\omega.S_f.(\alpha.D + S_B) + (-\alpha.D + S_f) \left[D.\sinh\left(\frac{H}{L_\omega}\right) + L_\omega.S_B.\cosh\left(\frac{H}{L_\omega}\right) \right] e^{-\alpha H} \right\}}{D.(1-\alpha^2.L_\omega^2) \left[L_\omega.D(S_B + S_f).\cosh\left(\frac{H}{L_\omega}\right) + (D^2 + S_f.S_B.L_\omega^2) \sinh\left(\frac{H}{L_\omega}\right) \right]} \quad (10)$$

Where S_f and S_B are respectively the recombination speed at the junction and to the rear side.

3. Photocourant Density

Knowing the expression of the minority density carriers, one can determine the expression of the photocurrent density by using the Fick law. It is given by the following equation:

$$J(S_f, S_b, \lambda, \omega, kl, \phi) = q.D. \left. \frac{\partial \delta(x, S_f, S_b, \lambda, \omega, kl, \phi)}{\partial x} \right)_{x=0} \quad (11)$$

all calculation done, we get:

$$J_{ph_2} = \frac{q \alpha I_0 (1-R) L^2}{(1-\alpha^2 L^2)} \left\{ \frac{\begin{aligned} & -L.S_F.(S_B + \alpha.D) + [L.\alpha.D(S_B + S_F) + .L.S_B.(S_F - \alpha.D)] \exp(-\alpha.H) \cosh\left(\frac{H}{L}\right) + \\ & [\alpha(D^2 + S_F.S_B.L^2) + D(S_F - \alpha.D)] \exp(-\alpha.H) \sinh\left(\frac{H}{L}\right) \end{aligned}}{L.D(S_F + S_B) \cosh\left(\frac{H}{L}\right) + (D^2 + S_F.S_B.L^2) \sinh\left(\frac{H}{L}\right)} \right\} \quad (12)$$

Where q is the charge of the electron and D the complex diffusion coefficient.

The photocurrent density according to the recombination velocity junction Sf_j and to backside Sb can be seen in figure 2.

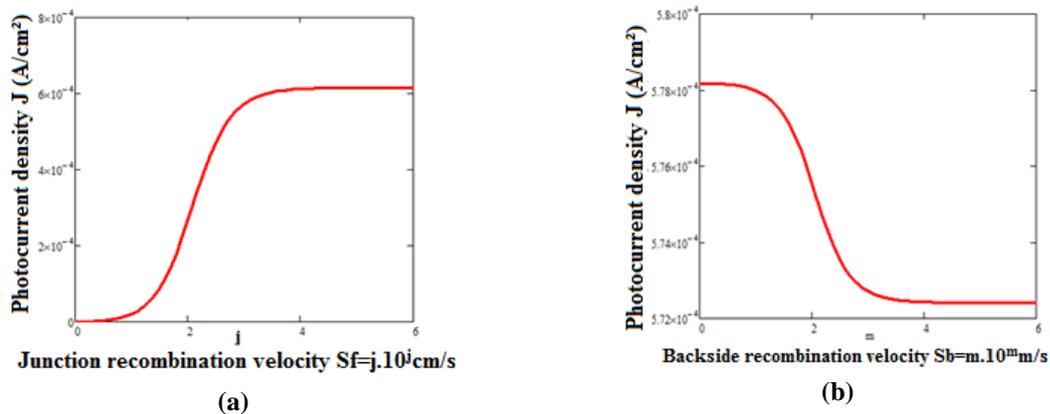


Figure 2: Modulus of the photocurrent density versus the junction recombination velocity Sf_j (a) and the backside recombination velocity Sb_m (b)

$$\lambda = 0.98 \mu\text{m} ; \omega = 10^6 \text{ rad} / \text{s} ; kl = 15 \text{ MeV}^{-1} . \text{s}^{-1} \phi = 150 \text{ MeV}$$

Plots of photocurrent density versus the recombination velocities (Sf and Sb) has a bearing for the high values of Sf (Sf ≥ 10⁵ cm / s) and Sb (Sb ≥ 10⁵ cm / s). Therefore, the zero gradient at that points lead to the expressions of the intrinsic recombination velocities through the junction and through the backside of the cell.

4. Expressions for Sf and Sb

Solving the equations (13) and (14) lead to the expressions of the recombination velocities Sf and Sb respectively [25-26].

$$\left[\frac{d[J_2(Sf, Sb, \lambda, \omega, kl, \phi)]}{d[Sb(\lambda, \omega, kl, \phi)]} \right]_{Sb \geq 10^5 \text{ cm} / \text{s}} = 0 \quad (13)$$

$$\left[\frac{d[J_2(Sf, Sb, \lambda, \omega, kl, \phi)]}{d[Sf(\lambda, \omega, kl, \phi)]} \right]_{Sf \geq 10^5 \text{ cm} / \text{s}} = 0 \quad (14)$$

After all calculation, one find:

$$Sf = \frac{D}{L_\omega} \times \frac{sh\left(\frac{H}{L_\omega}\right) + L_\omega \alpha \left(e^{-\alpha H} - ch\left(\frac{H}{L_\omega}\right) \right)}{L_\omega \alpha sh\left(\frac{H}{L_\omega}\right) - ch\left(\frac{H}{L_\omega}\right) + e^{-\alpha H}} \tag{15}$$

$$Sb = D \times \frac{\left(sh\left(\frac{H}{L_\omega}\right) + L_\omega \alpha ch\left(\frac{H}{L_\omega}\right) \right) e^{-\alpha H} - L_\omega \alpha}{\left(1 - ch\left(\frac{H}{L_\omega}\right) + L_\omega \alpha \times sh\left(\frac{H}{L_\omega}\right) \right) \times e^{-\alpha H} L_\omega} \tag{16}$$

5. Bode and Nyquist Plots Relating to Sf and Sb

The Bode and Nyquist plots [27-29] are used here to evaluate the impact of irradiation on the recombination velocities. And also, to describe the electrical phenomena of the intrinsic recombination velocities at the Junction Sf and to the backside Sb.

5.1. Bode Plots

Plots Bellow illustrate how the irradiation energy affect the recombination parameters.

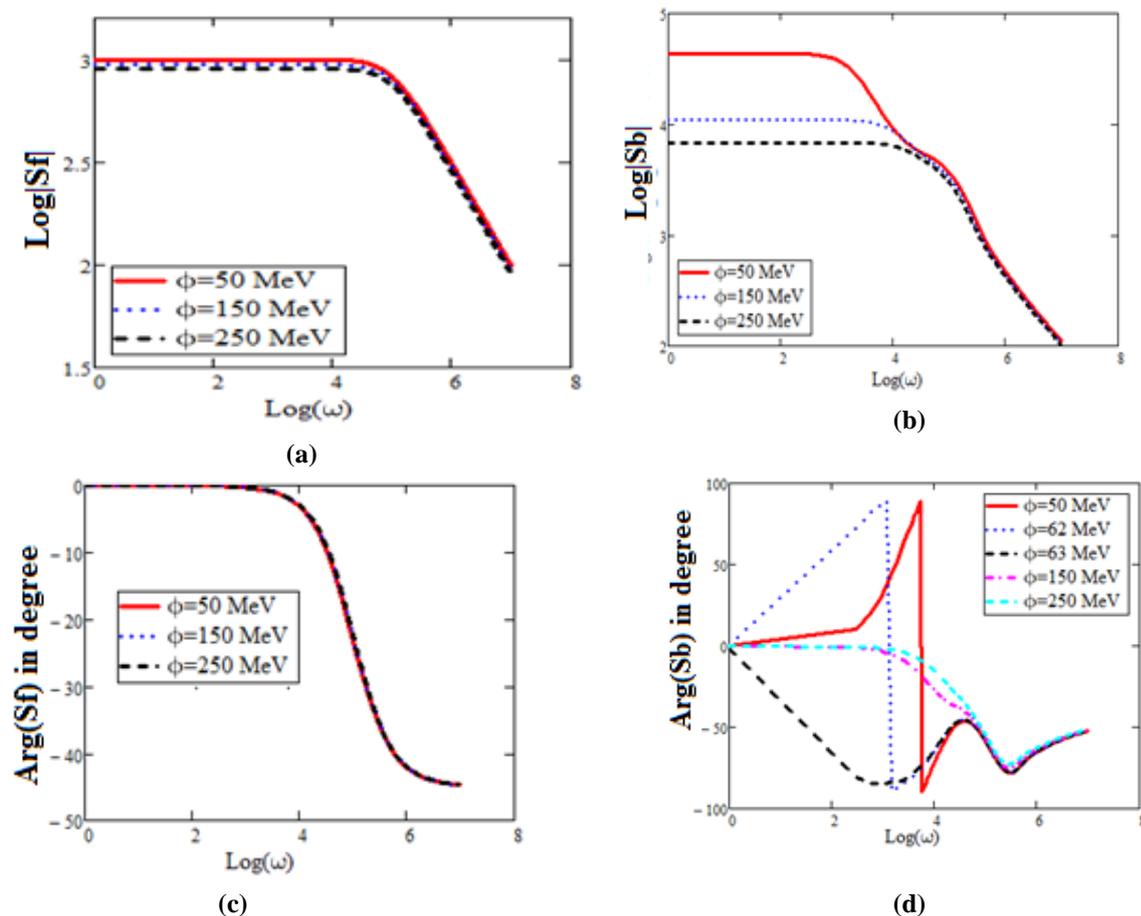


Figure 3: Bode plots for various irradiation values $\lambda = 0.98\mu\text{m}$; $kl = 15\text{MeV}^{-1}.\text{s}^{-1}$

Plots (a) and (b) show that the modulus of recombination velocities (Sf and Sb) is insensitive to the angular frequency as long as the latter is less than the quasi-static cut-off pulsation ωc , and beyond this pulsation, the modulus of Sb and Sf, very sensitive to the frequency, decreases abruptly according to the pulsation (dynamic frequency regime). High frequencies lead to small values of the recombination velocities, thus less losses of

minority carriers at the emitter-base and at the backside. Moreover, the effect of irradiation is more perceptible when operating in quasi-static regime and the more it increases, less important the recombination. Furthermore, the increase in irradiation results in an increase in the value of the cut-off frequency (boundary frequency between the quasi-static regime and the dynamic frequency regime, fig.a).

Figure (d) shows:

- For any given irradiation energy greater than or equal to 63 MeV, there is a pulsation below which the phase of the recombination velocity is nil. Beyond that pulsation, the phase decreases and remains negative so as to materialize a predominance of capacitive effects over inductive effects.
- For any irradiation energy, less than or equal to 62 MeV, the phase of the recombination velocity remains positive nearby the resonance and then becomes negative for higher frequencies: this describes both the inductive and capacitive phenomena of the backside recombination velocity.

The graph (c), shows that, regardless of the applied irradiation energy, there's always a predominantly capacitive effect.

5.2. Nyquist Plots for Sf and Sb

The impact of irradiation on the Nyquist plots is shown in the graphs below

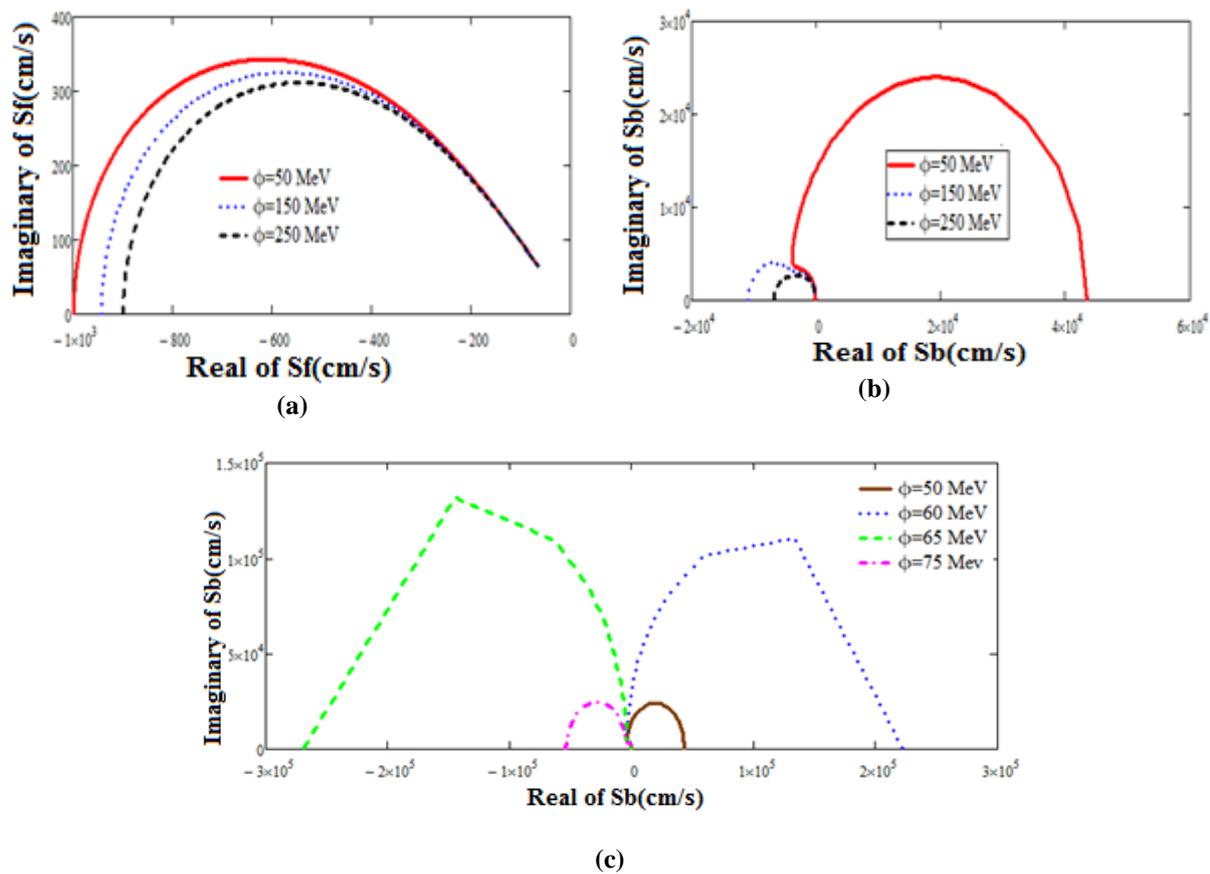


Figure 4: Nyquist plots for Sf (a) and for Sb (b, c) for various irradiation energy values $\lambda = 0.98 \mu\text{m}$;

$$kl = 15 \text{MeV}^{-1} \cdot \text{s}^{-1}$$

On these plots, you can see that they all are semi-closed loop curves of variable diameters depending on the value of the irradiation. Indeed, the greater the energy the greater the radius, characterizing both the capacitive and inductive phenomena of the recombination velocities Sb and Sf.



In concordance with the Bode diagram of Figure 3 (d), one can notice see that there is an energy above which the capacitive effects predominate over the inductive effects and below which these two effects coexist (Figure c).

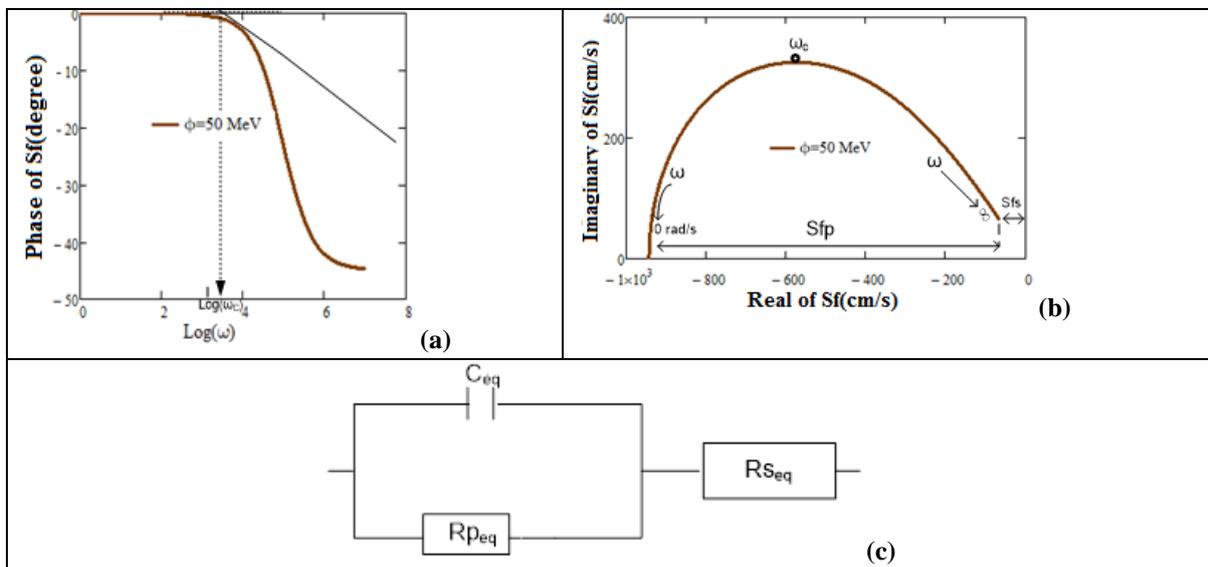
6. Equivalent Electrical Circuit Model for an Irradiation Energy Equal to 50 MeV

Based on the Nyquist and Bode plots, some equivalent electric models for the recombination velocities Sf and Sb at $\Phi=50$ MeV are proposed. And subsequently, a graphical method for determining equivalent electric parameters will be proposed too.

6.1. Junction Recombination Velocity Sf

An electrical circuit can be proposed based on the imaginary part of the junction recombination velocity vs its real part (see table 1

Table 1: equivalent electric circuit of Sf; $\lambda = 0.98\mu\text{m}$; $kl = 15\text{MeV}^{-1} \cdot \text{s}^{-1}$



The storage, the losses due to the recombination of the excess minority carriers through the emitter-base interface, can be electrically designed by a capacitance C, a shunt resistor Rp and a series resistance Rs respectively.

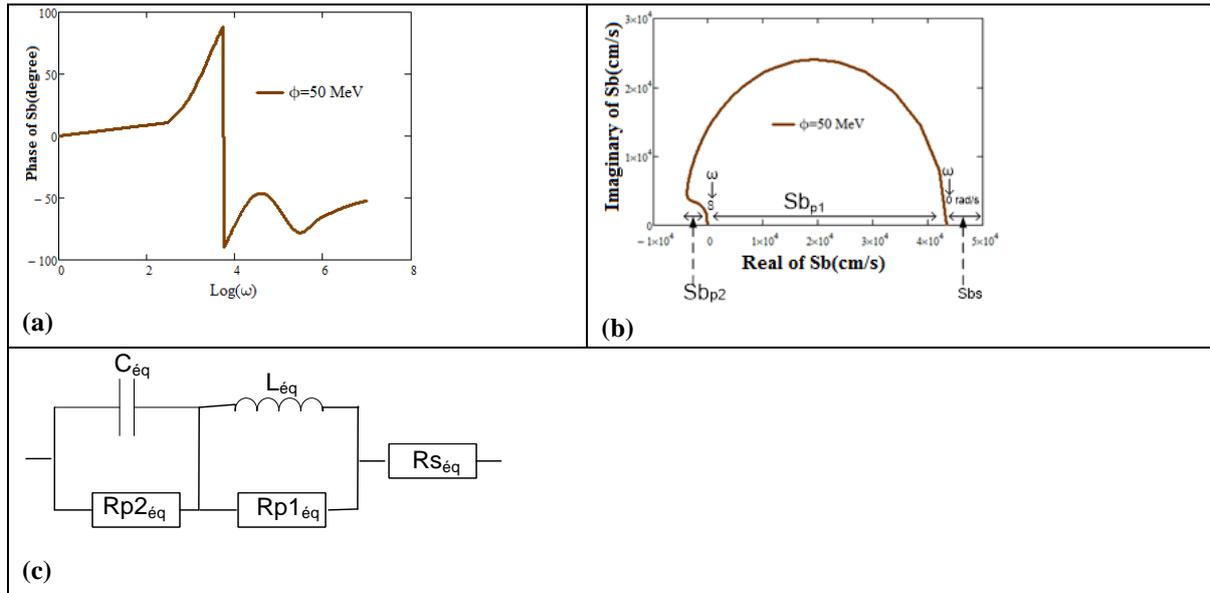
The equivalent electrical circuit (c) describes the electric behaviour of the recombination velocity through the junction Sf. The losses due to the recombination of the carriers through the emitter-base are assimilated to resistors.

C_{eq} is the capacitance of a capacitor which characterizes the capacitive effects of the recombination velocity Sf; R_{peq} , is a shunt resistance and R_{seq} is a series resistance. The values of the series resistance R_{seq} ($\omega \rightarrow 0$ or $\omega \rightarrow \infty$), shunt R_{peq} , (from the cut-off frequency giving $R_{peq} / 2$) can be evaluated using diagram (b). Knowing the value of the cut-off frequency, we can be deduced the value of the photogenerated minority carriers' lifetime and the capacitance from the relations $\tau = 1/\omega_c$ et $\tau = R_{peq} \cdot C_{eq}$ [30-31].

6.2. Backside Recombination Velocity Sb

An electric circuit can be proposed based on the imaginary part of the backside recombination velocity vs its real part (see table 2).

Table 2: equivalent electric circuit method for Sb $\lambda = 0.98\mu\text{m}$; $kl = 15\text{MeV}^{-1} \cdot \text{s}^{-1}$



Using the Nyquist plot (b), the equivalent electrical circuit (c) of the table2 describes the capacitive and inductive phenomena observed from the phase of S_b (a). C_{eq} represents the capacitive effects and L_{eq} the inductive effects. $R_{p1_{eq}}$ is a shunt resistance estimated when the excitation pulse $\omega \rightarrow 0$ and $\omega \rightarrow \infty$. and $R_{p2_{eq}}$ a shunt resistance corresponding to the diameter of the semicircle of the capacitive phenomenon.

We note that $R_{p2_{eq}}$ is less than $R_{p1_{eq}}$ but still when $R_{p2_{eq}}$ is zero, the inductive effects prevail. It is the same when the pulsation $\omega < 10^3$ rad / s. And in this frequency domain, the imaginary of S_b vs the logarithm of the pulsation is a straight line whose slope represents the equivalent inductance L_{eq} (diagram c).

6.3. Graphical method for determination of electric parameters ($R_{S_{eq}}$, $R_{p_{eq}}$ and L_{eq})

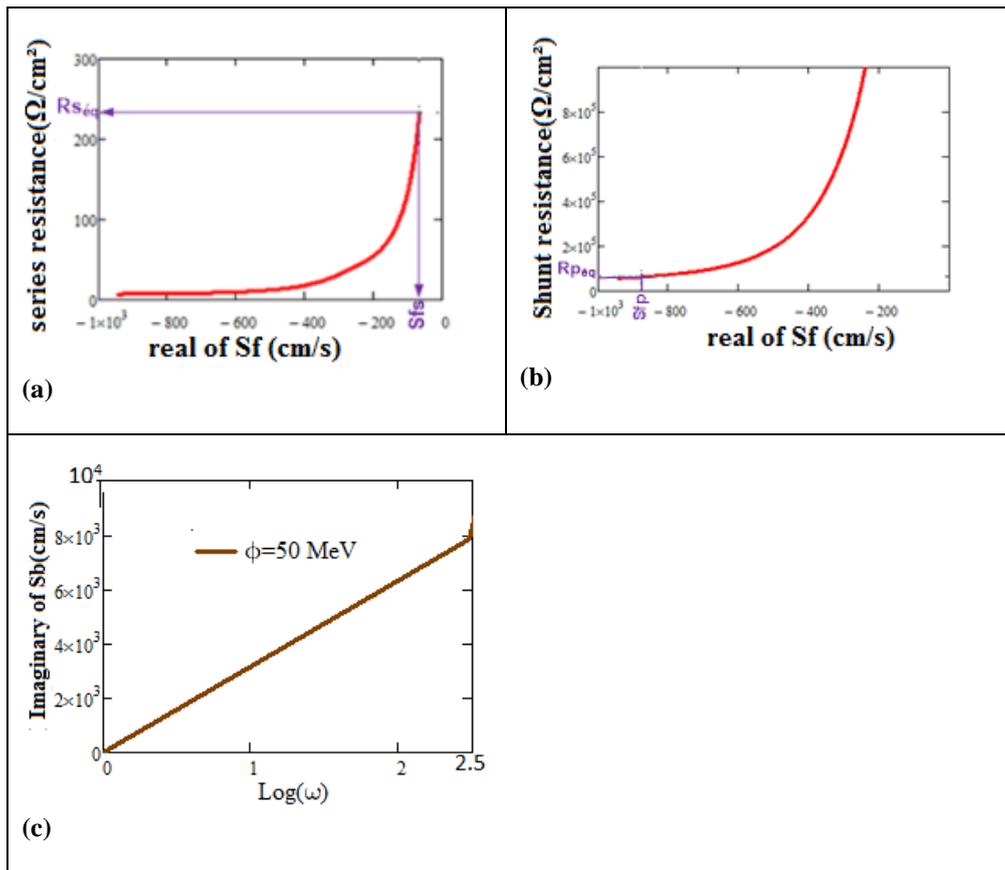
The method consists of representing the modulus of the series and shunt resistances vs the real part of S_f (or S_b). For each value of S_{fp} or S_{fs} (S_{bs} or S_{bp}) obtained, we proceed its projection on the curves then the y-intercepts (modulus of R_{series} or R_{shunt}) give the values of $R_{S_{eq}}$ or $R_{p_{eq}}$.

Whereas the slope of the imaginary of S_b vs the pulsation ($\omega < 10^3$) graph (c) (Table 3) gives the equivalent inductance L_{eq} , graph (c) Table 2.

Example: recombination velocity S_f

Table 3: evaluation method of electric parameters ($R_{S_{eq}}$, $R_{p_{eq}}$ and L_{eq})





For each value of S_{fs} or S_{fp} obtained from the Nyquist plot (Table 1) there is corresponding value of $R_{s_{eq}}$ or $R_{p_{eq}}$. Indeed:

- The diameter of the semicircle S_{fp} (diagrams b, Table 1) lead to the shunt resistance $R_{p_{eq}}$ (diagram c, table 1);
- S_{fs} , determined when $\omega \rightarrow 0$ or $\omega \rightarrow \infty$, lead to the equivalent series resistance $R_{s_{eq}}$ (graph c Table 1).

Knowing the value of the cut-off frequency, we can deduce the equivalent electrical capacitance from the equation $\tau = 1/\omega_c$ et $\tau = R_{p_{eq}} \cdot C_{eq}$.

The table 4 below gives values of the parameters mentioned above for three (3) irradiation energy values.

Table 4: values of Electric parameters

$\Phi(\text{MeV})$	$ S_{fs} (\text{cm/s})$	$ S_{fp} (\text{cm/s})$	$R_{s_{eq}}(\Omega/\text{cm}^2)$	$R_{p_{eq}}(\Omega/\text{cm}^2)$	$C_{eq}(\mu\text{F}/\text{cm}^2)$
50	69,314	993,086	13,988	13562	$2,331.10^{-2}$
150	66,392	926,71	14,964	15066	$2,099.10^{-2}$
250	64,055	874,825	15,866	16517	$1,914.10^{-2}$

when the irradiation energy values increase, the resistances $R_{s_{eq}}$ and $R_{p_{eq}}$ increase whereas the equivalent electrical capacitance decreases. This is due to the fact that the irradiation damages the material causing an increase in losses of minority carriers. The intrinsic properties of the solar cell are damaged; Resulting in poor cell quality.

The decrease of the capacitance was predictable since the capacitance is inversely proportional to the shunt resistance (which increases) according to the expression $C_{eq} = 1 / (R_{peq} * \omega c)$. In fact, the diffusion capacitance decreases since there are few of minority carriers diffusing in volume [32-33].

7. Conclusion

The recombination velocities of the bifacial silicon solar cell are very sensitive to the irradiation energy. Indeed, an increase in irradiation causes more losses of minority carriers. The negative impact of irradiation particles is more accentuated for the greater energy values. Then it is clear that even with the low values of energy, for a prolonged exposure to irradiations, the damage resulting from the impact of irradiation will be significant.

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